Saint-Petersburg State Polytechnic University



A.M.Levchenya, V.V.Ris, E.M.Smirnov

Test computations of turbulent flow in an axial-radial centrifugal compressor impeller using CFX-TASCflow package and a detailed analysis of tip-clearance effects

TESIS Moscow, 2003

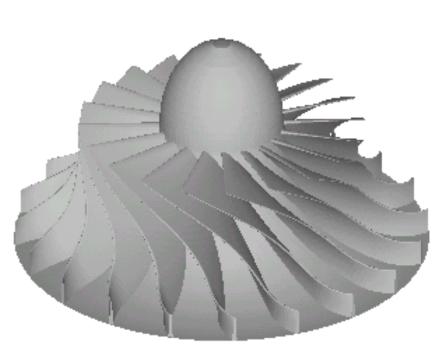
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- > Introduction
- > Experimental model and operating conditions
- > Numerical model, computational grid and cases considered
- > Results and discussion
- > Conclusions

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Experimental test description



Centrifugal compressor impeller (backswept rotor A: experiments by D.Eckardt et al, 1976-1980)

- ✓ 20 blades with sweep angle 60°
- ✓ Tip-clearance between shroud and blades:

 $0.5 \div 0.8$??

- ✓ Tip speed: $\approx 300 \text{ m/s}$
- ✓ Pressure ratio: 1.91
- ✓ Efficiency: 88.6%

Shaft speed: 14000 r.p.m.

Optimum air mass flow rate: 4.54 kg/s

Inlet total pressure: 101.33 kPa

Inlet total temperature: 15°C

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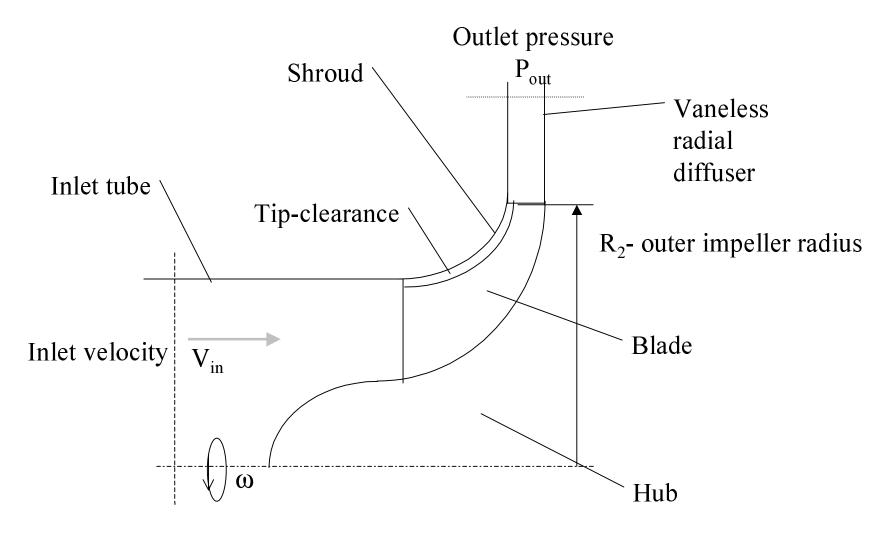
Mathematical model and computational aspects

- Reynolds-averaged Navier-Stokes and energy equation for turbulent compressible flow. Formulation in the reference frame rotating with the impeller
- $7 k-\omega$ turbulence model (Wilcox, 1993)

- **△** CFX-TASCflow package, version 1.21.1 Beta
- ≥ Multiblock structured grid created with software developed at the Department of Aerodynamics of SPSPU was converted to the CFX-TASCflow format
- ≥ Second order discretization scheme

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Meridional section of computational domain

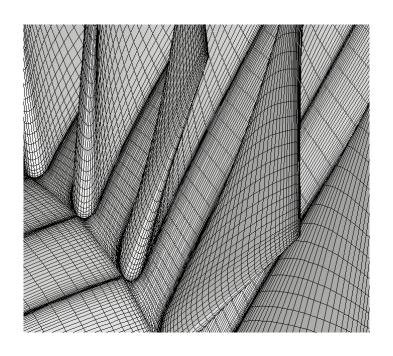


Computational grid at a meridional section

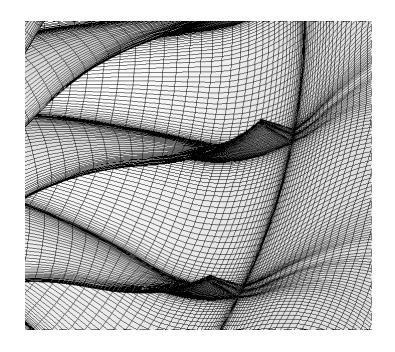
Number of grid nodes on main gridlines				
Main flow direction	130, including			
Inlet part	30	(0)(0)		
Blade passage	70		Vaneless	
Diffuser	30		radial	
From hub to shroud	48, including		diffuser	
Blade body	40		ulliusel	
Tip-clearance	8			
Between blades	40 - 60, including			
Inside blade passage	40			
In each of 2 additional blocks	10			
Inlet		Blade Number of grid no	odes for grid blocks	
	0 11			
	Overall g		273600, including	
		Inlet part	57600	
		Blade passage	134400	
		Three-block diffuser	57600 + 2x12000	

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Computational domain: grid aspects



Grid resolution near blade leading edge

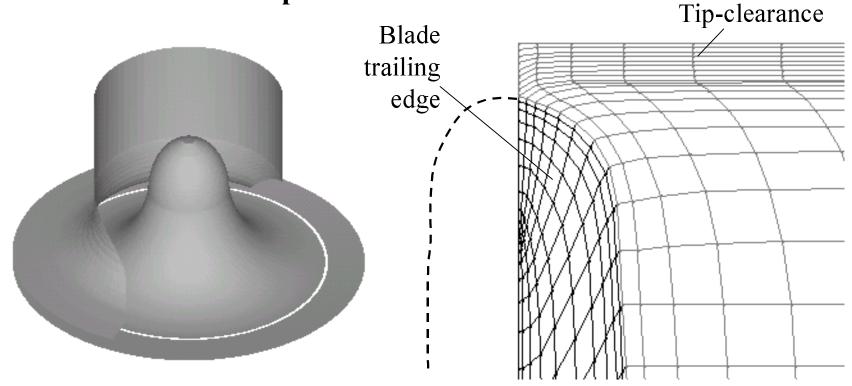


Grid resolution near blade trailing edge

Near-wall grid nodes are situated at distance $Y^+ \approx 10$

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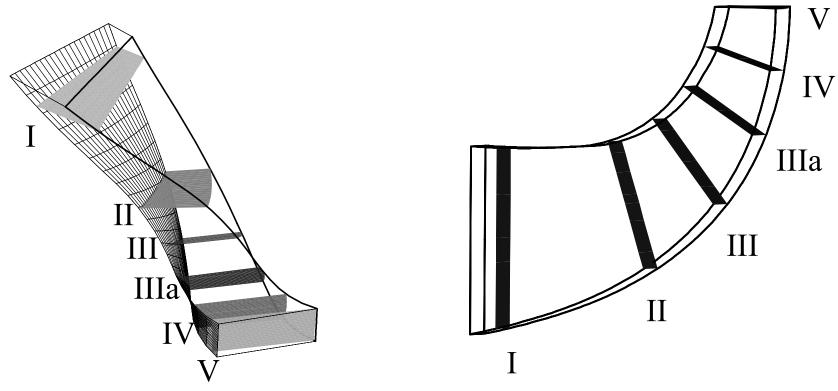
Computational domain features



A part of the flow domain, including the circular gap between the stationary diffuser wall and the rotating hub

Grid resolution near the tipclearance at impeller discharge CFX-TASCflow Slide 9 of 16

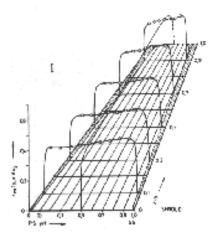
Flow analysis inside the blade passage



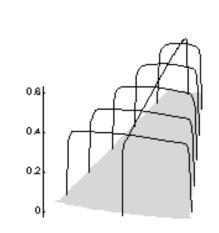
Two schemes defining passage cross-sections for velocity measurements *)

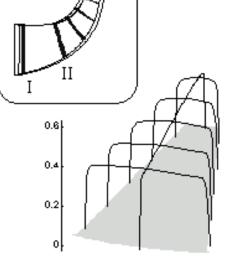
^{*)} Relative velocity on next slides is referred to impeller tip speed

Section I

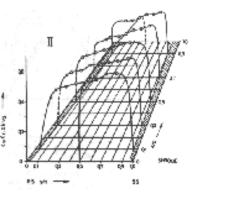


0.6 0.4 0.2 0





Section II

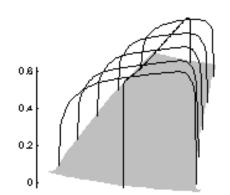


0.8 0.4 0.2

Full tip-clearance

0.6 0.4 0.2 0

50% tip-clearance



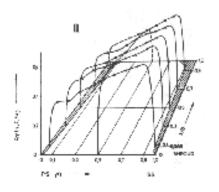
No tip-clearance

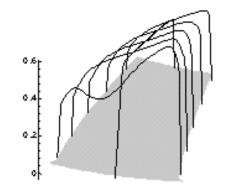
Experiment

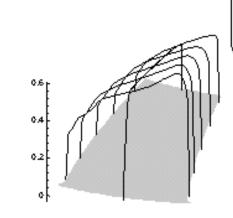
Results of computations

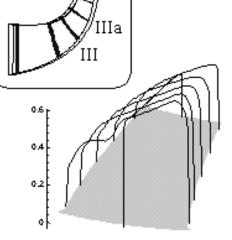
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Section III

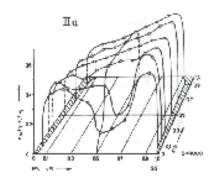


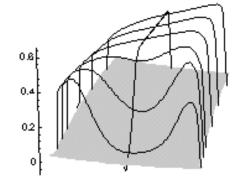


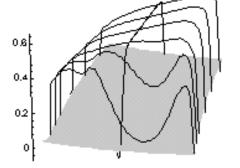


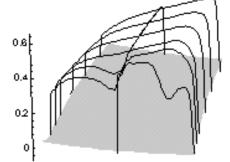


Section IIIa



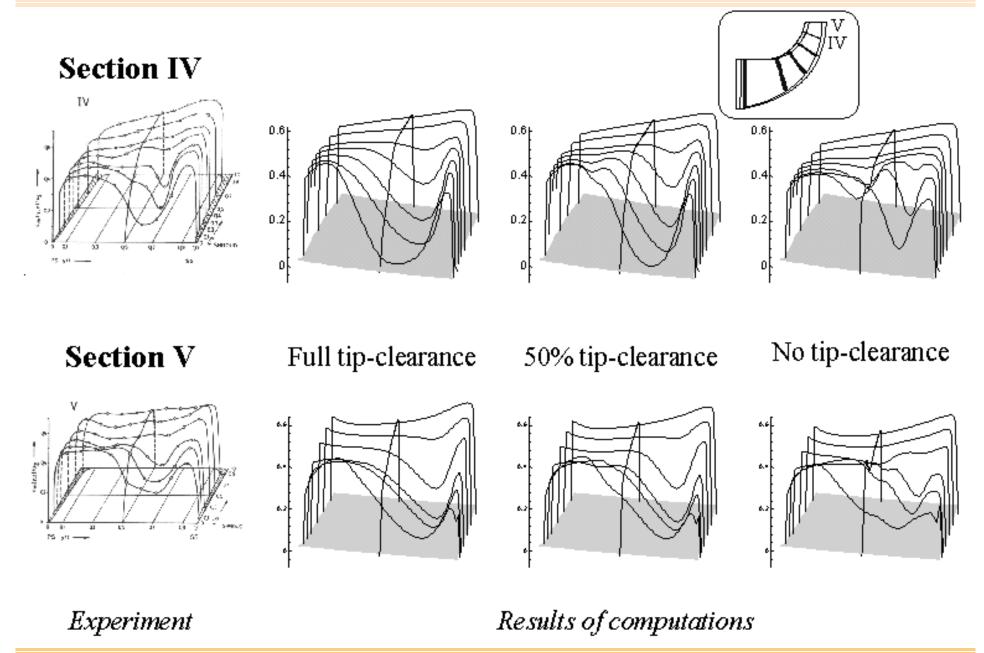






Experiment

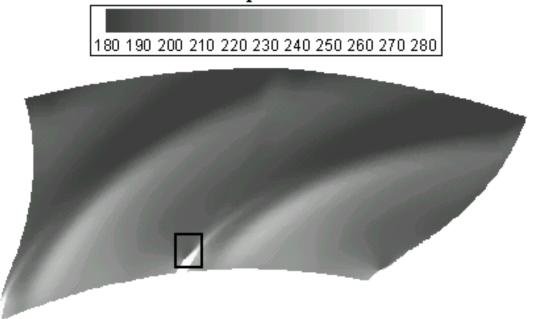
Results of computations



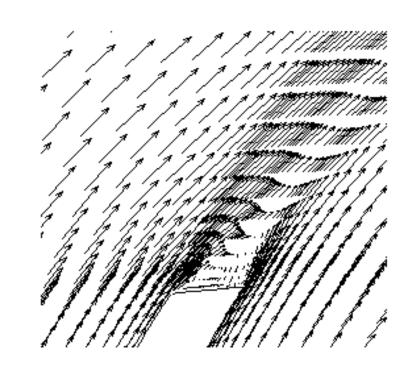
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Vaneless diffuser flow

meters per second



Distribution of absolute velocity at mid-width diffuser section



Relative velocity vectors near blade trailing edge

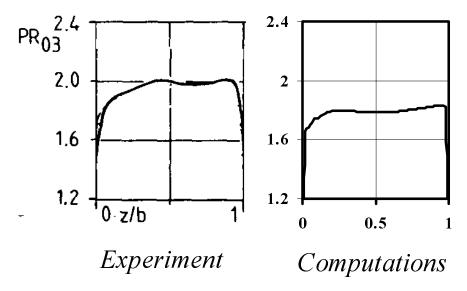
Comparison of integral characteristics

	Pressure ratio	Efficiency		
Experiment	1.91	88.6%		
Computations:				
Full tip-clearance	1.81	92.9%		
50% tip-clearance	1.84	93.8%		
No tip-clearance	1.87	95.1%		

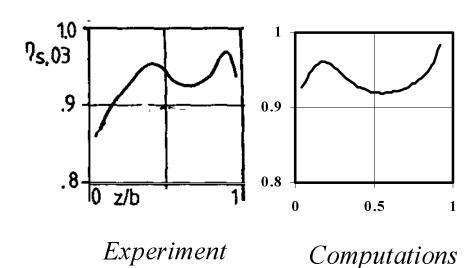
$$PR_{03} = \frac{P_{1.075R_2}}{P_{in}}$$

$$\eta_{s,03} = \frac{k-1}{k} \cdot \frac{ln \ PR_{03}}{ln \frac{T_{ex}}{T_{in}}}$$

Total pressure profiles at impeller discharge



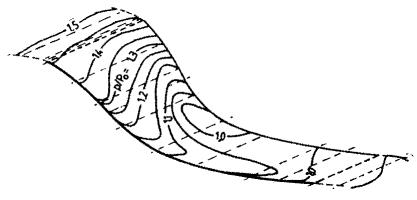
Efficiency profiles at impeller discharge



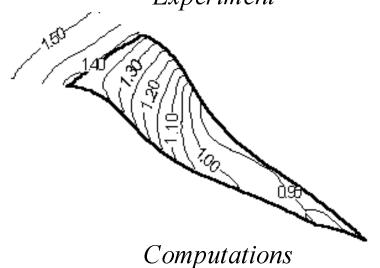
Pressure fields for the flow with 50% tip-clearance

(values referred to inlet total pressure)

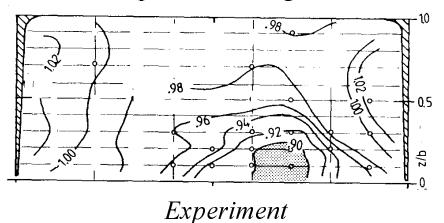
Static pressure on the shroud



Experiment



Relative total pressure distribution at impeller discharge



0.98

Computations

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Conclusions

→ Parametric computations of three-dimensional turbulent flow in a high-speed centrifugal compressor backswept impeller were performed.

- → Computational results for local and integral characteristics were compared with data of widely known experiments.
- → The tip-clearance width, varied in the present computations, has a small influence on overall performance. Efficiency is overpredicted, and the outlet-to-inlet pressure ratio is underpredicted in all the cases computed.
- → The best agreement between the measured and computed velocity fields was achieved when the tip-clearance value was set to 50% of the value measured in the experiments under non-rotating impeller conditions.